



Block Diagram Piezodrive for Nanophysics and Nanotechnology

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Abstract

The piezodrive is used in nanophysics and nanotechnology, scanning microscopy, delivery DNA, compound telescope, interferometer and adaptive optics. The method mathematical physics is used to construct the block diagram of the piezodrive from the equation of reverse piezo effect and its ordinary differential equation for nanophysics and nanotechnology. The matrix transfer function of the piezodrive is obtained. The block diagrams of the piezodrive with the back electromotive force at distributed and lumped parameters are determined for nanophysics and nanotechnology.

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Introduction

The piezodrive is used for actuation of systems for nanophysics, nanotechnology, displacement and delivery DNA, compound telescope, interferometer, adaptive optics, scanning microscopy. This piezodrive is used to actuate or control nano mechanisms and convert electrical energy to mechanical energy at the nano displacement [1-17]. By method mathematical physics the block diagram of the piezodrive is determined for nanophysics and nanotechnology. The block diagram of the piezodrive is determined and show the transformation of electrical energy into mechanical energy in difference from Cady's and Mason's equivalent circuits [18-41]. The block diagram of the piezodrive for nanophysics and nanotechnology is determined with using the equation of reverse piezo effect and its linear ordinary second-order differential equation. From this set of equations for the block diagram of the piezodrive the matrix transfer function is determined [34-47]. For nanophysics and nanotechnology, the matrix transfer function of the piezodrive is obtained.

Method

The parameters of the piezodrive for nanophysics and nanotechnology are obtained by method mathematical

physics with using the equation the inverse piezo effect and its ordinary second-order differential equation.

The transverse inverse piezoeffect [1-10] is written as.

$$S_1 = d_{31}E_3 + s_{11}^E T_1,$$

Block diagram of a nano piezo engine for nanobionics and longitudinal inverse piezo effect as

$$S_3 = d_{33}E_3 + s_{33}^E T_3,$$

where $S_1, S_3, d_{31}, d_{33}, E_3, s_{11}^E, s_{33}^E, T_1, T_3$ are the relative deformation along axes 1 and 3, the transverse and longitudinal piezo modules, the electric field strength along axes 3, the elastic compliances at the transverse and longitudinal piezo effect at $E = \text{const}$ and the mechanical stress along axes 1 and 3.

Then the equation for the inverse piezo effect for the piezodrive has the general form [1 - 10]

$$S_i = s_{ij}^\Psi T_j + v_{mi} \Psi_m,$$

here $s_{ij}^\Psi = \{s_{33}^E, s_{11}^E, s_{55}^E, s_{33}^D, s_{11}^D, s_{55}^D - \text{the elastic compliances,}$
 $v_{mi} = \{d_{33}, d_{31}, d_{15}, g_{33}, g_{31}, g_{15} - \text{the piezoelectric constant,}$
 $\Psi_m = \{E_3, E_3, E_1, D_3, D_3, D_1 - \text{the control parameter: } E - \text{electric field strength, } D - \text{the electric induction, } \gamma - \text{the coefficient of wave propagation, } i = 1, 2, \dots, 6, j = 1, 2, \dots, 6, m = 1, 2, 3.$

The ordinary second-order differential equation for the piezodrive in nanophysics and nanotechnology has the form [11–19]

$$\frac{d^2 \Xi(x,p)}{dx^2} - \gamma^2 \Xi(x,p) = 0.$$

Block Diagram

By method mathematical physics the block diagram of the piezodrive is calculated for nanophysics and nanotechnology. The method mathematical physics is used to construct the block diagram of the piezodrive for nanophysics and nanotechnology from the equation of the reverse piezo effect and its ordinary differential equation.

The solution of the ordinary second-order differential equation the piezodrive for nanophysics and nanotechnology has the form

$$\Xi(x,p) = C e^{-\gamma x} + B e^{\gamma x}; \gamma = p/c^\Psi + \alpha$$

here $\Xi(x,p)$ - the Laplace transform of the displacement; x - the coordinate; p - the operator, the coefficient of propagation, c^Ψ - the speed of sound and α - the coefficient of damping.

Its coefficients C and B are derived

$$C = \frac{\Xi_1 e^{\gamma l} - \Xi_2}{2 \text{sh}(\gamma l)}; B = \frac{\Xi_2 - \Xi_1 e^{-\gamma l}}{2 \text{sh}(\gamma l)}.$$

This solution of the ordinary second-order differential equation the piezodrive for nanophysics and nanotechnology has the form

$$\Xi(x,p) = \frac{\Xi_1(p) \text{sh}[\gamma(l-x)] + \Xi_2(p) \text{sh}(\gamma x)}{2 \text{sh}(\gamma l)}.$$

The equations of the forces at the faces for the piezodrive are determined in the form

$$T_j(0, p)S_0 = F_1(p) + M_1p^2\Xi_1(p) \text{ at } x = 0;$$

$$T_j(l, p)S_0 = -F_2(p) - M_2p^2\Xi_2(p) \text{ at } x = l.$$

The equations for the mechanical stresses at the faces for the piezodrive are derived

$$T_j(0, p) = \frac{1}{s_{ij}^\Psi} \frac{d\Xi(x, p)}{dx} \Big|_{x=0} - \frac{\nu_{mi}}{s_{ij}^\Psi} E_m(p);$$

$$T_j(l, p) = \frac{1}{s_{ij}^\Psi} \frac{d\Xi(x, p)}{dx} \Big|_{x=l} - \frac{\nu_{mi}}{s_{ij}^\Psi} E_m(p).$$

We have the block diagram at the distributed parameters for the piezodrive in nanophysics and nanotechnology on Figure 1

$$\Xi_1(p) = [1/(M_1p^2)] \left\{ -F_1(p) + (1/\chi_{ij}^\Psi) \times [v_{mi}\Psi_m(p) - [\gamma/\text{sh}(\gamma l)][\text{ch}(\gamma l)\Xi_1(p) - \Xi_2(p)]] \right\};$$

$$\Xi_2(p) = [1/(M_2p^2)] \left\{ -F_2(p) + (1/\chi_{ij}^\Psi) \times [v_{mi}\Psi_m(p) - [\gamma/\text{sh}(\gamma l)][\text{ch}(\gamma l)\Xi_2(p) - \Xi_1(p)]] \right\};$$

here $\chi_{ij}^\Psi = s_{ij}^\Psi/S_0$.

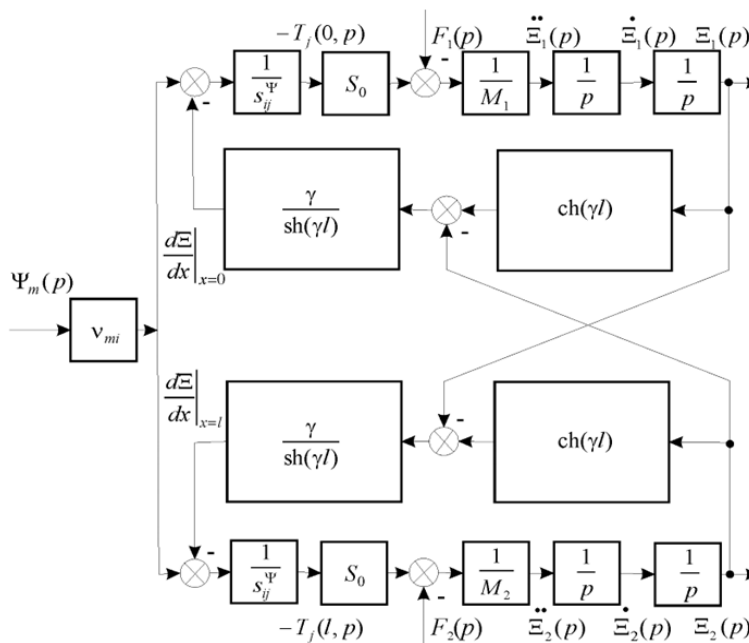


Figure 1: Block diagram piezodrive for nanophysics and nanotechnology.

From the block diagram at the distributed parameters for the piezodrive in nanophysics and nanotechnology on Figure 1 we have the equations

$$\Xi_1(p) = W_{11}(p)\Psi_m(p) + W_{12}(p)F_1(p) + W_{13}(p)F_2(p);$$

$$\Xi_2(p) = W_{21}(p)\Psi_m(p) + W_{22}(p)F_1(p) + W_{23}(p)F_2(p),$$

and the matrix equation for the piezodrive with its matrix transfer function

$$\begin{pmatrix} \Xi_1(p) \\ \Xi_2(p) \end{pmatrix} = \begin{pmatrix} W_{11}(p) & W_{12}(p) & W_{13}(p) \\ W_{21}(p) & W_{22}(p) & W_{23}(p) \end{pmatrix} \begin{pmatrix} \Psi_m(p) \\ F_1(p) \\ F_2(p) \end{pmatrix}$$

where the elements of the matrix are determined in the form

$$\begin{aligned} W_{11}(p) &= \Xi_1(p)/\Psi_m(p) = -\frac{v_{mi}[M_2\chi_{ij}^\Psi p^2 + \gamma \text{th}(\gamma l/2)]}{A_{ij}}; \chi_{ij}^\Psi = s_{ij}^\Psi/S_0; \\ A_{ij} &= M_1 M_2 (\chi_{ij}^\Psi)^2 p^4 + \{(M_1 + M_2)\chi_{ij}^\Psi/[c^\Psi \text{th}(\gamma l)]\} p^3 + \\ &+ [(M_1 + M_2)\chi_{ij}^\Psi \alpha/\text{th}(\gamma l) + 1/(c^\Psi)^2] p^2 + 2\alpha p/c^\Psi + \alpha^2; \\ W_{21}(p) &= \Xi_2(p)/\Psi_m(p) = \frac{v_{mi}[M_1\chi_{ij}^\Psi p^2 + \gamma \text{th}(\gamma l/2)]}{A_{ij}}; \\ W_{12}(p) &= \Xi_1(p)/F_1(p) = -\frac{\chi_{ij}^\Psi [M_2\chi_{ij}^\Psi p^2 + \gamma \text{th}(\gamma l/2)]}{A_{ij}}; \\ W_{13}(p) &= \Xi_1(p)/F_2(p) = W_{22}(p) = \Xi_2(p)/F_1(p) = \frac{\chi_{ij}^\Psi \gamma}{A_{ij} \text{sh}(\gamma l)}; \\ W_{23}(p) &= \Xi_2(p)/F_2(p) = -\frac{\chi_{ij}^\Psi [M_1\chi_{ij}^\Psi p^2 + \gamma \text{th}(\gamma l/2)]}{A_{ij}}. \end{aligned}$$

Discussion

At inertial load the static absolute displacements for the piezodrive in nanophysics and nanotechnology are derived in the form

$$\begin{aligned} |\xi_1(\infty)| &= d_{33}U (M_2 + m/2)/(M_1 + M_2 + m), \\ |\xi_2(\infty)| &= d_{33}U (M_1 + m/2)/(M_1 + M_2 + m), \\ |\xi_1(\infty)| + |\xi_2(\infty)| &= d_{33}U, \end{aligned}$$

here m, M_1, M_2 are the masses of the piezo engine and loads. For the PZT piezodrive at $m \rightarrow 0$ at $d_{33} = 0.4 \text{ nm/V}$, $U = 100 \text{ V}$, $M_1 = 0.5 \text{ kg}$ and $M_2 = 2 \text{ kg}$ we obtain the parameters $|\xi_1(\infty)| = 32 \text{ nm}$, $|\xi_2(\infty)| = 8 \text{ nm}$, $|\xi_1(\infty)| + |\xi_2(\infty)| = 40 \text{ nm}$.

For the piezodrive at the voltage control the electromechanical coupling coefficient has form

$$k_{mi} = \frac{d_{mi}}{\sqrt{s_{ij}^E \varepsilon_{mk}^T}}$$

The negative feedback for the block diagram at the distributed parameters and voltage control of the piezodrive on Figure 2 has the form

$$U_{\Xi a}(p) = \frac{d_{mi} S_0 R}{\delta s_{ij}^E} \dot{\Xi}_a(p), \quad a = 1, 2.$$

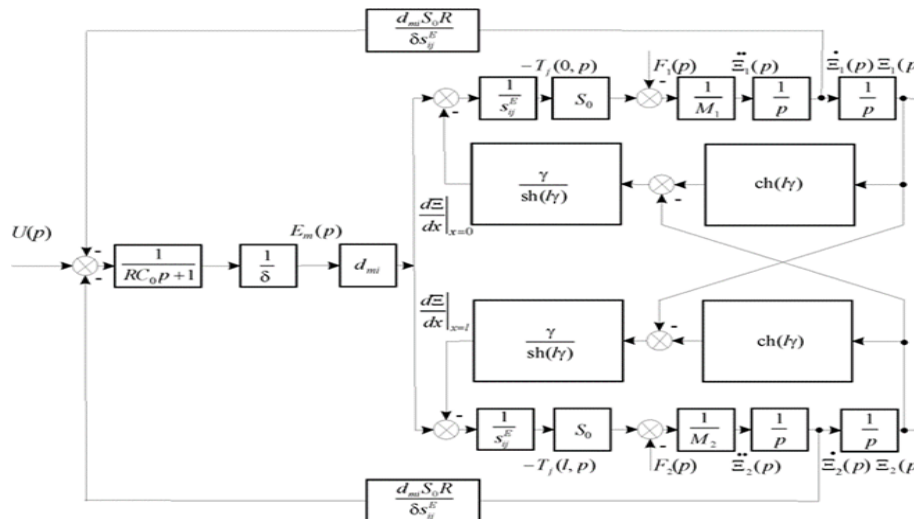


Figure 2: Block diagram piezodrive at voltage control and distributed parameters with negative feedbacks.

Let us consider the block diagrams with lumped parameters. For the piezodrive its block diagrams with lumped parameters at the voltage control are on Figure 3 and at the current control on Figure 4 for one fixed face of the piezodrive.

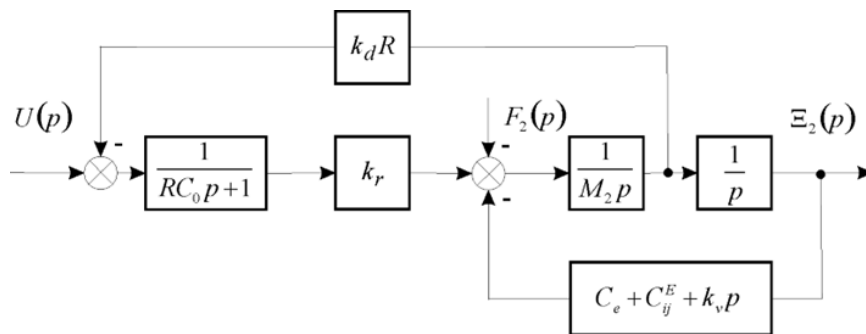


Figure 3: Block diagram piezodrive at one rigidly fixed face and voltage control for lumped parameters.

The coefficient k_d is equal to the coefficient k_r on Figure 3 and Figure 4

$$k_d = k_r = \frac{d_{mi} S_0}{\delta S_{ij}^\Psi}$$

where $\Psi = E, D$ are its upper indexes.

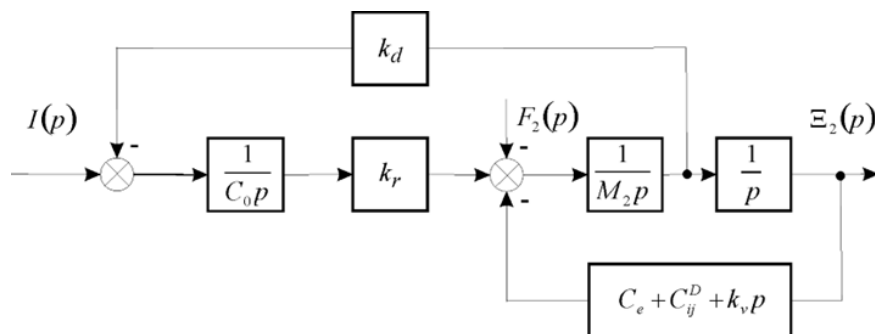


Figure 4: Block diagram piezo engine at current control and lumped parameters.

Therefore, we have the block diagrams for the piezodrive in nanophysics and nanotechnology.

Conclusion

The block diagram for the piezodrive is determined for nanophysics and nanotechnology. The block diagram, the matrix transfer function of the piezodrive are derived. The numerical parameters of the piezodrive are determined. Its block diagrams with the back electromotive force at distributed and lumped parameters are derived for nanophysics and nanotechnology.

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